

# Polyhedral Cylinders Formed by Kokotsakis Meshes

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*Dedicated to Prof. Kuno Egle, Karlsruhe Institute of Technology*

**Abstract.** Kokotsakis proved that an infinite planar mesh composed of congruent convex, non-trapezoidal, non-parallelogramic quadrilaterals is deformable with degree of freedom 1 in two modes if the quadrilaterals are rigid and if the edges are revolute joints. Stachel proved that in the deformed state the vertices of all quadrilaterals are located on a circular cylinder the radius of which is a free parameter. In other words: A Kokotsakis mesh forms two polyhedral cylinders which are deformable with degree of freedom one. Later, Stachel also investigated under which conditions a polyhedral cylinder is tiled by quadrilaterals. In the present paper new proofs and new results are obtained by using special parameters for quadrilaterals in combination with cylinder coordinates.

*Key Words:* Kokotsakis mesh, spherical four-bar, polyhedral cylinder, foldable and self-intersecting tiled polyhedral cylinder, periodic polyhedral cylinder, deltoid, parabola through four points

*MSC 2020:* 52C25 (primary), 51M20, 70B15

## 1 Kokotsakis Mesh

A Kokotsakis mesh is an infinite planar tessellation composed of congruent convex, non-trapezoidal, non-parallelogramic quadrilaterals (Figure 1). The exclusion of trapezoids and parallelograms is explained further below. The internal angles in the representative quadrilateral  $V_0V_1V_2V_3$  add up to  $2\pi$ :  $\alpha_0 + \alpha_1 + \alpha_2 + \alpha_3 = 2\pi$ , so that only three angles  $\alpha_1, \alpha_2, \alpha_3$  are independent. As parameters of the quadrilateral the side lengths  $V_0 - V_1 = \ell$ ,  $V_0 - V_3 = a$ ,  $V_1 - V_2 = b$  and the lengths  $V_0 - V_2 = d_1$  and  $V_1 - V_3 = d_2$  of the diagonals 1 and 2 are used. These parameters determine the side length  $V_2 - V_3 = c$  and the internal angles.

By reflecting one or both of the triangles  $V_0V_1V_2$  and  $V_0V_1V_3$  in a side other quadrilaterals with the same lengths  $\ell, a, b, d_1, d_2$  are obtained. In these quadrilaterals  $V_0 - V_2$  and  $V_1 - V_3$  are not both diagonals.

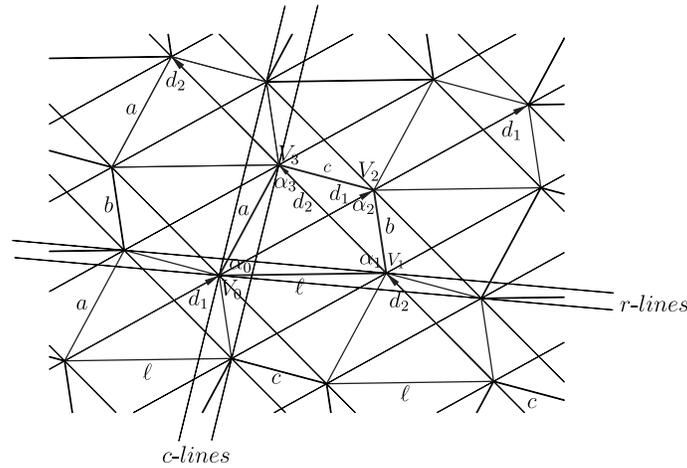


Figure 1: Kokotsakis mesh. Parameters  $\ell, a, b, d_1, d_2$  and internal angles  $\alpha_k$  of the representative quadrilateral  $V_0V_1V_2V_3$ . Sets 1 and 2 of parallel diagonals. Rows and columns of quadrilaterals.  $r$ -lines and  $c$ -lines.

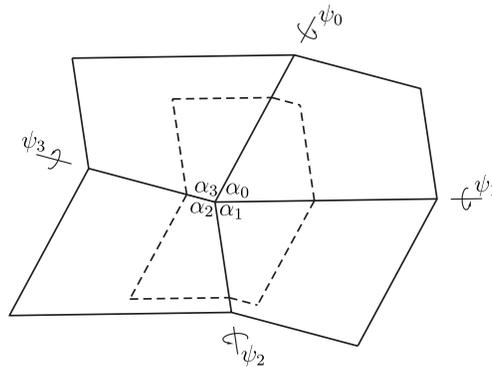


Figure 2: Spherical four-bar, parameters  $\alpha_k$ , variables  $\psi_k$  ( $k = 0, 1, 2, 3$ ).

By the diagonals two sets of parallel straight lines with equidistant vertices are defined, the distance being  $d_1$  on one set and  $d_2$  on the other.

In the mesh *rows* and *columns* of quadrilaterals are distinguished. Adjacent rows are separated by a zigzagging line of alternating lengths  $\ell, c, \ell, c$  etc. Adjacent columns are separated by a zigzagging line of alternating lengths  $a, b, a, b$  etc. The quadrilateral in row  $i$  and column  $j$  is called  $q_{ij}$  with  $q_{00}$  being an arbitrarily chosen quadrilateral.

By the boundaries of rows and columns two more sets of parallel straight lines with equidistant vertices are defined. In Figure 1 they are denoted  $r$ -lines and  $c$ -lines.

The mesh is invariant with respect to

- (a)  $180^\circ$ -rotations about the midpoints of sides of quadrilaterals
- (b) translations  $m\vec{d}_1$  and  $n\vec{d}_2$  along the diagonals ( $m, n = 0, \pm 1, \pm 2, \dots$ ).

By the translations  $m\vec{d}_1$  and  $n\vec{d}_2$  the quadrilateral  $q_{ij}$  ( $i, j$  arbitrary) is displaced into the position of the quadrilateral  $q_{uv}$  with  $u = i + m + n$  and  $v = j + m - n$ .

Every vertex of the mesh is center of a *cluster* of four quadrilaterals. Every quadrilateral is part of four clusters. All clusters are congruent. A single isolated cluster (the solid lines in Figure 2) represents a spherical four-bar mechanism. Parameters are the three independent internal angles  $\alpha_1, \alpha_2, \alpha_3$ . Variables are the fold angles  $\psi_0, \psi_1, \psi_2, \psi_3$  indicated in the figure (zero in the flat position). Provided the quadrilaterals are neither trapezoids nor

parallelograms a given angle  $\psi_0$  determines two (not necessarily real) sets of angles  $\psi_1, \psi_2, \psi_3$  (Wittenburg [5]). Hence the four-bar is a single-degree-of-freedom mechanism with two modes of deformation. If  $(\psi_0, \psi_1, \psi_2, \psi_3)$  is a state of deformation, then also  $(-\psi_0, -\psi_1, -\psi_2, -\psi_3)$  is.

Two types of spherical four-bars are distinguished (see [5, pp. 641–643]):

Type I: All fold angles are subject to the constraint  $|\psi_i| < \pi$ . No two quadrilaterals of the spherical four-bar can intersect each other.

Type II: A single fold angle  $\psi_k$  is unconstrained. Up to  $\psi_k = \pi$  deformation is possible by folding. Beyond  $\psi_k = \pi$  two opposite quadrilaterals of the spherical four-bar intersect each other. Realisation requires to interpret the spherical four-bar as truss made of rods which can be dis-assembled and re-assembled. Since every vertex in Figure 1 is center of a spherical four-bar, intersections result in highly complicated three-dimensional trusses.

The dashed lines in Figure 2 point to the fact that quadrilaterals having the same internal angles result in different meshes with identical relationships between fold angles.

## 2 Cylinder Coordinates

Kokotsakis [2] proved

**Theorem 1.** *A mesh is deformable in two different modes.*

Stachel [3, 4] proved

**Theorem 2.** *In the deformed state the vertices of all quadrilaterals are located on a circular cylinder the radius  $r$  of which is a free parameter.*

In the geometrical proofs given in [2] and [3, 4] neither parameters of quadrilaterals nor cylinder coordinates of vertices are used. In what follows new proofs are given.

First, it is shown that the vertices of a single quadrilateral  $V_0V_1V_2V_3$  can be located on a circular cylinder of arbitrary (not arbitrarily small) radius  $r$ . The vertices are points on the ellipse in which plane and cylinder intersect. Let  $r, \varphi_k, z_k$  ( $k = 0, 1, 2, 3$ ) be the cylinder coordinates of  $V_k$ . Cartesian coordinates of the position vector  $\vec{r}_k$  of  $V_k$  are

$$\vec{r}_k = [r \cos \varphi_k, r \sin \varphi_k, z_k]. \tag{1}$$

Without loss of generality  $\varphi_0 = z_0 = 0$ , so that there are seven unknowns  $r, \varphi_k, z_k$  ( $k = 1, 2, 3$ ). These seven unknowns are subject to only six constraint equations expressing the prescribed lengths  $\ell, a, b, d_1, d_2$  and the planarity condition  $(\vec{r}_1 - \vec{r}_0) \cdot [(\vec{r}_2 - \vec{r}_0) \times (\vec{r}_3 - \vec{r}_0)] = 0$ . The square of the distance of two vertices  $V_i$  and  $V_j$  on the cylinder is  $(\vec{r}_i - \vec{r}_j)^2 = 2r^2[1 - \cos(\varphi_i - \varphi_j)] + (z_i - z_j)^2$ . The six constraint equations are

$$2r^2(1 - \cos \varphi_1) + z_1^2 = \ell^2, \tag{2}$$

$$2r^2(1 - \cos \varphi_2) + z_2^2 = d_1^2, \tag{3}$$

$$2r^2(1 - \cos \varphi_3) + z_3^2 = a^2, \tag{4}$$

$$2r^2[1 - \cos(\varphi_1 - \varphi_2)] + (z_1 - z_2)^2 = b^2, \tag{5}$$

$$2r^2[1 - \cos(\varphi_1 - \varphi_3)] + (z_1 - z_3)^2 = d_2^2, \tag{6}$$

$$\sum_{i=1}^3 z_i [\sin \varphi_j - \sin \varphi_k - \sin(\varphi_j - \varphi_k)] = 0 \quad (i, j, k = 1, 2, 3 \text{ cyclic}). \tag{7}$$

As predicted, the radius  $r$  is a free parameter.

Two vertices on the cylinder define the helix passing through these vertices. The equidistant vertices on the two sets of parallel lines along the diagonals 1 and 2 in Figure 1 are mapped into equidistant vertices on two sets of parallel helices. Because of the invariance property (a) of the planar mesh the deformed mesh is invariant with respect to turning the cylinder upside down. Translatory displacements  $m\vec{d}_1$  and  $n\vec{d}_2$  of quadrilaterals along the diagonals in the planar mesh are mapped into screw displacements  $(m\varphi_2, mz_2)$  and  $[n(\varphi_3 - \varphi_1), n(z_3 - z_1)]$ , respectively, the screw axis being the cylinder axis. The resultant screw displacement is  $[m\varphi_2 + n(\varphi_3 - \varphi_1), mz_2 + n(z_3 - z_1)]$ .

The resultant screw displacement has no effect on the state of deformation of the cluster of four quadrilaterals shown in Figure 2. From this it follows that in the deformed state of the mesh all clusters are congruent. Since a single cluster has two modes of deformation, the mesh as a whole has two modes of deformation. This proves the existence of two polyhedral cylinders (PCs) mobile with degree of freedom one and specified by roots  $\varphi_{k1,2}(r)$ ,  $z_{k1,2}(r)$  ( $k = 1, 2, 3$ ) of the equations. This concludes the proof.

The minimal radius  $r_{\min}$  allowing real solutions is determined in Section 3. If Equations (2)–(7) are solved by  $(z_1, z_2, z_3)$ , then also by  $(-z_1, -z_2, -z_3)$ , and if they are solved by  $(\varphi_1, \varphi_2, \varphi_3)$ , then also by  $(-\varphi_1, -\varphi_2, -\varphi_3)$ . Relevant solutions are those for which  $V_0 - V_2$  and  $V_1 - V_3$  are diagonals of the quadrilateral.

Equations (2)–(7) cannot be decoupled. This is true also for equations resulting from the transformation  $u_k = \tan \varphi_k/2$ ,  $1 - \cos \varphi_k = 2u_k^2/(1 + u_k^2)$ ,  $\sin \varphi_k = 2u_k/(1 + u_k^2)$ .

Special case: A quadrilateral inscribed in a circle of radius  $\varrho$  is specified by the polar coordinates  $\beta_1, \beta_2, \beta_3$  of  $V_1, V_2, V_3$ , respectively. In these terms  $\ell^2 = 2\varrho^2(1 - \cos \beta_1)$ ,  $d_1^2 = 2\varrho^2(1 - \cos \beta_2)$ ,  $a^2 = 2\varrho^2(1 - \cos \beta_3)$ ,  $b^2 = 2\varrho^2[1 - \cos(\beta_1 - \beta_2)]$ ,  $d_2^2 = 2\varrho^2[1 - \cos(\beta_1 - \beta_3)]$ . With these parameters Equations (2)–(7) have with  $r = \varrho$  in both modes of deformation the solution  $z_k = 0$ ,  $\varphi_k = \beta_k$  ( $k = 1, 2, 3$ ). This state of deformation cannot be produced by folding the mesh.

The outward normal vector of the quadrilateral  $V_0V_1V_2V_3$  is  $(\vec{r}_1 - \vec{r}_0) \times (\vec{r}_2 - \vec{r}_0)$ . The scalar product of the unit normal vectors of two quadrilaterals sharing an edge is the cosine of the fold angle in this edge (one of the angles  $\psi_k$  ( $k = 0, 1, 2, 3$ )). For all quadrilaterals the cosine of the angle between the cylinder axis and the normal to the quadrilateral is equal in magnitude and alternating in sign along rows and along columns.

In every state of deformation of a mesh the projections of all quadrilaterals along the cylinder axis are congruent quadrilaterals inscribed in a circle. The projected quadrilaterals are divided into two groups of equidistant quadrilaterals, the angular distance being  $\varphi_2$  in one group and  $\varphi_3 - \varphi_1$  in the other. For being convex it is necessary and sufficient that

$$\text{either } 0 < \varphi_1 < \varphi_2 < \varphi_3 \quad \text{or} \quad 0 < \varphi_3 < \varphi_2 < \varphi_1. \quad (8)$$

By the inequality signs the case is excluded that the projected quadrilaterals are secants of the circle. This case is the subject of Section 6.1 on trapezoidal quadrilaterals.

Let angles  $\varphi_1, \varphi_2, \varphi_3$  satisfying the convexity condition (8) and parameters  $z_1, z_2$  (or  $z_1, z_3$ ) and  $\ell > |z_1|$  be arbitrarily prescribed. With these data Equations (2)–(7) determine the parameters  $z_3$  (or  $z_2$ ),  $r$ ,  $d_1$ ,  $a$ ,  $b$  and  $d_2$  specifying a quadrilateral  $V_0V_1V_2V_3$  and a state of deformation of the mesh. With the parameters  $\ell, d_1, a, b, d_2$  of the quadrilateral the variables  $\varphi_{k1,2}, z_{k1,2}$  ( $k = 1, 2, 3$ ) can then be calculated numerically as functions of  $r$ .

*Example 1.* The prescribed data  $\varphi_1 = 180^\circ$ ,  $\varphi_2 = 90^\circ$ ,  $\varphi_3 = 60^\circ$ ,  $z_1 = 1/2$ ,  $z_3 = 1$ ,  $\ell = 1$  determine  $z_2 = (3 + 7\sqrt{3})/12$ ,  $r = \sqrt{3}/4$ ,  $d_1^2 = (7/24)(5 + \sqrt{3})$ ,  $b^2 = (7/24)(5 - \sqrt{3})$ ,

$a = \sqrt{19}/4$ ,  $d_2 = \sqrt{13}/4$ . The unit outward normal vector has the cartesian coordinates  $\sqrt{1/61}[-\sqrt{3}, 7, -3]$ . From five unit normal vectors the fold angles are calculated:  $\cos \psi_0 = 53/61$ ,  $\cos \psi_1 = 37/61$ ,  $\cos \psi_2 = (14\sqrt{3} - 9)/61$ ,  $\cos \psi_3 = (16\sqrt{3} - 9)/61$ .  $\diamond$

### 3 Geometrical Solution

In every state of deformation of a mesh all quadrilaterals are circumscribed by congruent ellipses. Figure 3 shows a quadrilateral  $V_0V_1V_2V_3$  and a circumscribing ellipse with semi axes  $a$  and  $b < a$  (not to be confused with the parameters  $a, b$  in Figure 1). The radius  $r$  of the cylinder is  $b$ , and its axis is tilted against the plane of the ellipse by the angle  $\alpha = \arctan(b/a)$  shown in the figure. The cylinder coordinates  $\varphi_k, z_k$  ( $k = 0, 1, 2, 3$ ) are found by projections as is demonstrated by  $\varphi_0, z_0$ . The vertex  $V_k$  ( $k = 0, 1, 2, 3$ ) on the ellipse and its axial projection on the circle are located on one and the same side of the minor principal axis of the ellipse. By the angles  $\varphi_0, \varphi_1, \varphi_2, \varphi_3$  the projection of the quadrilateral onto the circle is determined. Every ellipse circumscribing the quadrilateral determines cylinder coordinates  $r, \varphi_k, z_k$  ( $k = 0, 1, 2, 3$ ) defining a state of deformation of the mesh.

In what follows, all ellipses circumscribing a given quadrilateral are determined in analytical form. For better understanding it is helpful to make a sketch of two parabolas 1 and 2 intersecting each other in four points and of the quadrilateral  $V_0V_1V_2V_3$  defined by these points. Everything which follows ( $x, y$ -axes, domains, ellipses in these domains, lines  $y = \text{const}$ ) should be marked in this sketch.

By the  $x, y$ -coordinates of  $V_0, V_1, V_2, V_3$  in some arbitrarily chosen  $x, y$ -system and by the coordinates  $x_4, y_4$  of an additional auxiliary point  $P$  a second-order curve circumscribing the quadrilateral is defined. Its equation is

$$\det \begin{bmatrix} x^2 & y^2 & xy & x & y & 1 \\ x_0^2 & y_0^2 & x_0y_0 & x_0 & y_0 & 1 \\ x_1^2 & y_1^2 & x_1y_1 & x_1 & y_1 & 1 \\ x_2^2 & y_2^2 & x_2y_2 & x_2 & y_2 & 1 \\ x_3^2 & y_3^2 & x_3y_3 & x_3 & y_3 & 1 \\ x_4^2 & y_4^2 & x_4y_4 & x_4 & y_4 & 1 \end{bmatrix} = 0. \tag{9}$$

In the  $x, y$ -system with  $V_0$  as origin and with  $V_2$  on the  $x$ -axis this equation reads

$$x_2 \cdot \det \begin{bmatrix} y^2 & xy & x & y \\ y_1^2 & x_1y_1 & x_1 & y_1 \\ y_3^2 & x_3y_3 & x_3 & y_3 \\ y_4^2 & x_4y_4 & x_4 & y_4 \end{bmatrix} - \det \begin{bmatrix} x^2 & y^2 & xy & y \\ x_1^2 & y_1^2 & x_1y_1 & y_1 \\ x_3^2 & y_3^2 & x_3y_3 & y_3 \\ x_4^2 & y_4^2 & x_4y_4 & y_4 \end{bmatrix} = 0.$$

This is the equation  $A(x^2 - x_2x) + 2Bxy + Cy^2 + Ey = 0$  with coefficients  $A, B, C, E$  which are second-order functions of  $x_4, y_4$ .  $P$  determines an ellipse if  $AC - B^2 > 0$ .

The fourth-order equation  $AC - B^2 = 0$  separating ellipses from hyperbolas is the equation of the two parabolas passing through the vertices of the quadrilateral. Let  $(\varrho_1, \gamma)$  and  $(\varrho_2, \gamma)$  be the polar coordinates of these parabolas. Substitution of  $x_4 = \varrho \cos \gamma$ ,  $y_4 = \varrho \sin \gamma$  results in a quadratic equation with real roots  $\varrho_{1,2}(\gamma)$ . For geometrical constructions of the parabolas see [1, Example 7.4.1].

Let  $\Delta_1$  be the domain inside parabola 1,  $\Delta_2$  be the domain inside parabola 2 and  $\Delta_{12}$  be the intersection of  $\Delta_1$  and  $\Delta_2$ . The curve is an ellipse if  $P$  is located either in  $\Delta_1$  or in

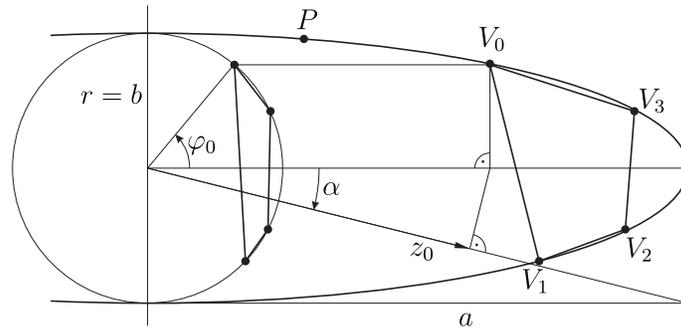


Figure 3: Quadrilateral  $V_0V_1V_2V_3$  and auxiliary point  $P$  defining a circumscribing ellipse. Cylinder coordinates  $r$  and  $\varphi_0$ ,  $z_0$  of  $V_0$ . Projected quadrilateral.

$\Delta_2$ , but not in  $\Delta_{12}$ . The sketch shows that every ellipse is located in  $\Delta_1$  as well as in  $\Delta_2$ . Slender ellipses have the most part of their circumference either in  $\Delta_1$  or in  $\Delta_2$ . Slender ellipses occur when the planar mesh is only slightly deformed. Hence the conclusion: Each mode of deformation is associated with one parabola and with a family of ellipses. When the deformed mesh becomes planar, the ellipses tend, in the limit, toward the parabolas. With increasing deformation of the mesh the tilt angle  $\alpha$  and with it the ratio  $b/a = \tan \alpha$  is increasing, while the radius  $b$  of the cylinder is decreasing.  $b$  is calculated from  $A$ ,  $B$ ,  $C$ ,  $E$  as function of  $x_4$  and  $y_4$ . It suffices to calculate  $b$  for all points  $(x_4, y_4)$  of a straight line  $y = \text{const}$  which intersects all ellipses (in points other than  $V_1, V_2, V_3$ ). Then,  $b$  is a function of the single variable  $x_4$ . The minimum  $b_{\min}$  of this function is the minimal radius  $r_{\min}$  for which Equations (2)–(7) have a real solution  $\varphi_k, z_k$  ( $k = 1, 2, 3$ ).

The principal-axes system of an ellipse is inclined against the  $x, y$ -system by the angle  $\beta = (1/2) \arctan[2B/(A - C)]$ . In general,  $\beta$  depends on  $x_4, y_4$ . In the special case of quadrilaterals inscribed in a circle,  $2\beta$  is, independent of  $x_4, y_4$ , the angle enclosed by the diagonals of the quadrilateral:  $\tan 2\beta = (y_3 - y_1)/(x_3 - x_1)$ . The equation of the circumcircle is  $2B = A - C = 0$ . As was said already, the flat position of the mesh inside this circle cannot be produced by folding the mesh.

## 4 Tiled Polyhedral Cylinders

An infinite mesh is wrapped around a cylinder of arbitrary radius  $r$  infinitely many times. A polyhedral cylinder is said to be tiled if integers  $m$  and  $n$  exist such that the resultant screw displacement  $[m\varphi_2 + n(\varphi_3 - \varphi_1), mz_2 + n(z_3 - z_1)]$  equals  $(2\pi, 0)$ . This is the set of *closure conditions* (compare Stachel [4])

$$m\varphi_2 + n(\varphi_3 - \varphi_1) = 2\pi, \quad mz_2 + n(z_3 - z_1) = 0 \quad (m, n \text{ integer}). \quad (10)$$

On a tiled PC with integers  $(m, n)$  the quadrilateral  $q_{ij}$  ( $i, j$  arbitrary) coalesces with all quadrilaterals  $q_{uv}$  with  $u = i + k(m + n), v = j + k(m - n)$  ( $k = \pm 1, \pm 2, \dots$ ).  $m$  and  $n$  may be positive, zero or negative. The equations show:

1.  $(z_3 - z_1)/z_2$  is rational.
2. Reversing the signs of  $m, n, \varphi_k, z_k$  ( $k = 1, 2, 3$ ) has no effect on the tiled PC.
3. Replacing  $n$  by  $-n$ ,  $V_1$  by  $V_3$  and  $V_2$  by  $V_3$  has no effect on the tiled PC.
4. Tiled PCs are flatfolded if  $|m| + |n| = 2$ . They are three-dimensional if  $|m| + |n| \geq 3$ .
5. On a tiled PC with integers ( $m \geq 3, n = 0$ ) every string of  $m$  diagonals  $d_1$  connecting two vertices is mapped into a regular polygon with  $m$  sides of length  $d_1$  in a plane

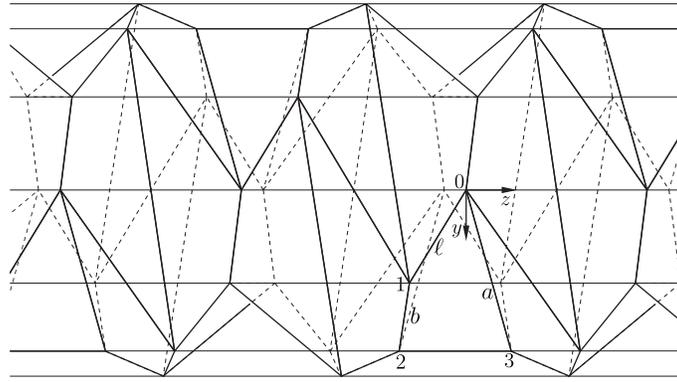


Figure 4: The foldable tiled PC of Example 2.

$z = \text{const}$ . Likewise, on a tiled PC with integers ( $m = 0, n \geq 3$ ) every string of  $n$  diagonals  $d_2$  connecting two vertices is mapped into a regular polygon with  $n$  sides of length  $d_2$  in a plane  $z = \text{const}$ .

6. A tiled PC is formed by  $|m + n|$  rows of quadrilaterals if  $m \neq 0$  and  $mn \geq 0$ . It is formed by  $|m - n|$  columns of quadrilaterals if  $n \neq 0$  and  $mn \leq 0$ .

Equations (2)–(7) and (10) are eight equations for the nine unknowns  $m, n, r, \varphi_k, z_k$  ( $k = 1, 2, 3$ ). Necessary conditions on the five parameters  $\ell, a, b, d_1, d_2$  for the existence of a solution are not available.

Tiled PCs can be constructed as follows. Integers  $m, n$  and angles  $\varphi_1, \varphi_2, \varphi_3$  satisfying the convexity condition (8) and the first Equation (10) are arbitrarily prescribed. In addition, one of the coordinates  $z_1, z_2, z_3$  and either the radius  $r$  or one of the lengths  $\ell, d_1, a, b, d_2$  are prescribed. Equation (7) and the second Equation (10) determine the unknowns among  $z_1, z_2, z_3$ . Finally, Equations (2)–(6) determine the squares of the remaining unknowns. If one of the lengths  $\ell, d_1, a, b, d_2$  is prescribed, then it must be sufficiently large so as to determine a value  $r^2 > 0$ . Whether a tiled PC constructed this way can be produced by folding the mesh or whether it is self-intersecting must be investigated separately.

A tiled PC is said to be M-periodic if a (smallest) integer  $M$  exists such that the screw displacements  $M(\varphi_2, z_2)$  and  $M(\varphi_3 - \varphi_1, z_3 - z_1)$  are both pure translations. Hence  $M\varphi_2$  and  $M(\varphi_3 - \varphi_1)$  must both be integer multiples of  $2\pi$ . Rationality of  $\varphi_2/\pi$  is a necessary and sufficient condition for periodicity. Periodicity means that every quadrilateral is periodically repeated in translation along the cylinder axis.

*Example 2.* Given are  $m = 3, n = 2, \varphi_1 = 30^\circ, \varphi_2 = 60^\circ, \varphi_3 = 120^\circ, z_1 = -1/2, \ell = 1$ .

The tiled PC determined by these data is M-periodic with  $M = 12$ . The data yield  $z_2 = -2(12 + 5\sqrt{3})/69 \approx -.5988, z_3 = (1 + 10\sqrt{3})/46 \approx .3983, r = (3\sqrt{2} + \sqrt{6})/4 \approx 1.6730, d_1^2 = (10690 + 5401\sqrt{3})/(12 \cdot 23^2), d_1 \approx 1.7770, a^2 = (9823 + 4781\sqrt{3})/(4 \cdot 23^2), a \approx 2.9250, b^2 = (1327 - 70\sqrt{3})/(3 \cdot 23^2), b \approx .8716, d_2^2 = 3(1204 + 609\sqrt{3})/(2 \cdot 23^2), d_2 \approx 2.5308$ .

In Figure 4 the tiled PC is shown in projection onto the  $y, z$ -plane. It is formed by folding  $m + n = 5$  rows of quadrilaterals. The periodic repetition of quadrilaterals in translation along the cylinder axis is clearly visible.  $\diamond$

*Example 3.* The data  $m = 8, n = -4, \varphi_1 = 60^\circ, \varphi_2 = 120^\circ, \varphi_3 = 210^\circ, z_3 = 1, r = 1$  determine the tiled PC with the parameters  $M = 12, z_1 = (25 - 14\sqrt{3})/37 \approx .0203, z_2 = (6 + 7\sqrt{3})/37 \approx .4898, \ell^2 = 2(1291 - 350\sqrt{3})/37^2, \ell \approx 1.0002, d_1^2 = 6(715 + 14\sqrt{3})/37^2, d_1 \approx 1.8000, a^2 = 3 + \sqrt{3}, a \approx 2.1753, b^2 = (3053 - 798\sqrt{3})/37^2, b \approx 1.1047, d_2^2 = 5(694 + 341\sqrt{3})/37^2, d_2 \approx 2.1661$ .

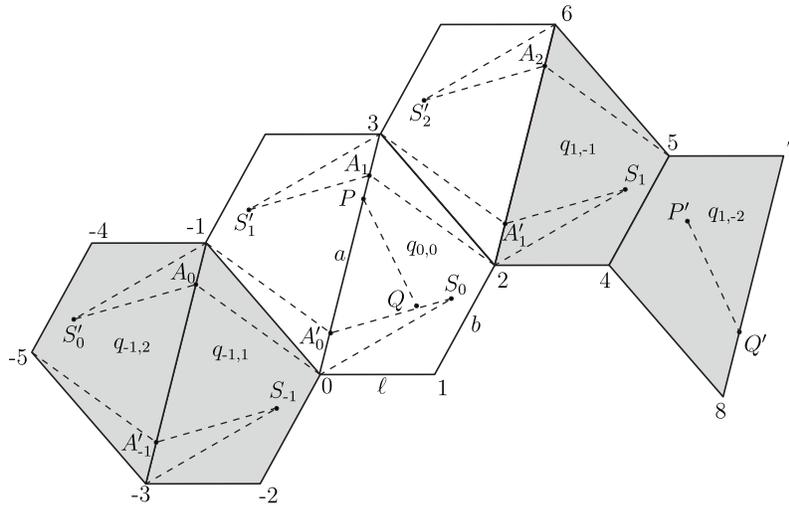


Figure 5: The planar mesh of Example 3. On the tiled PC the quadrilateral  $V_0V_1V_2V_3$  is intersected by the four shaded quadrilaterals in the dashed line segments.

This tiled PC which is formed by  $m-n = 12$  columns of quadrilaterals cannot be produced by folding the mesh. In Figure 5 the mesh is shown. On the tiled PC every quadrilateral is intersected in like manner by four other quadrilaterals. The quadrilateral  $V_0V_1V_2V_3$  labeled  $q_{0,0}$  is intersected by the four shaded quadrilaterals  $q_{-1,1}$ ,  $q_{1,-1}$ ,  $q_{-1,2}$  and  $q_{1,-2}$ . A point  $S_0$  inside  $q_{0,0}$  is intersected by the edge  $V_{-1} - V_{-3}$  at a point  $A_0$  on this edge. The equation  $\vec{r} = \vec{r}_{-1} + \mu(\vec{r}_{-3} - \vec{r}_{-1})$  of the edge with parameter  $\mu$  and the equation  $\vec{m} \cdot \vec{r} = 1$  of the plane with  $\vec{m}$  given by  $\vec{r}_0, \vec{r}_1, \vec{r}_2$  determine  $\mu$  and the positions of  $A_0$  and  $S_0$ :  $\mu \approx .1699$ , distances  $V_0 - A_0 = V_0 - S_0 \approx 1.3264$ ,  $V_3 - S_0 \approx 1.5636$ . The quadrilaterals  $q_{0,0}$  and  $q_{-1,1}$  intersect in the dashed line segments  $V_0 - A_0$  and  $V_0 - S_0$ .

All pairs of quadrilaterals sharing a single vertex intersect in like manner. This explains the dashed line segments  $A_1 - V_2 - S_1$ ,  $A'_1 - V_3 - S'_1$ ,  $A_0 - V_{-1} - S'_0$  etc.  $S'_0$  coalesces with  $A'_0$  and  $A_0$  with  $S_0$ . Hence  $q_{0,0}$  is intersected by  $q_{-1,2}$  in the dashed line segment  $S_0 - A'_0$ .

In the same way it is shown that  $q_{0,0}$  and  $q_{1,-2}$  intersect in the dashed line segments  $P - Q$  and  $P' - Q'$ . Distances:  $V_0 - P = V_7 - Q' \approx 2.1753$ ,  $V_0 - Q = V_7 - P' \approx 1.0155$ ,  $V_3 - Q = V_8 - P' \approx 1.5675$ .  $\diamond$

### 5 Deltoids

In this section a two-parametric family of deltoids forming tiled PCs with prescribed integers  $(m, n)$  is determined. A deltoid is a quadrilateral with mutually orthogonal diagonals one of which, say  $V_1 - V_3$ , is an axis of symmetry. Then,  $\ell = b$  and  $(\vec{r}_2 - \vec{r}_0) \cdot (\vec{r}_3 - \vec{r}_1) = 0$ . With (1), (2) and (5) these equations are

$$2r^2[\cos \varphi_1 - \cos(\varphi_1 - \varphi_2)] + z_2(z_2 - 2z_1) = 0, \tag{11}$$

$$r^2[\cos \varphi_1 - \cos(\varphi_1 - \varphi_2) - \cos \varphi_3 + \cos(\varphi_2 - \varphi_3)] + z_2(z_3 - z_1) = 0. \tag{12}$$

The second equation is replaced by a linear combination of both equations:

$$2r^2[\cos \varphi_3 - \cos(\varphi_2 - \varphi_3)] + z_2(z_2 - 2z_3) = 0. \tag{13}$$

From the fact that a diagonal cannot be on a generator of the cylinder and from the orthogonality of the diagonals it follows that  $z_2 \neq 0$ . Therefore, elimination of  $r^2$  from (11) and (13) results in

$$z_2[\cos \varphi_3 - \cos(\varphi_2 - \varphi_3) - \cos \varphi_1 + \cos(\varphi_1 - \varphi_2)] + 2\{z_3[\cos \varphi_1 - \cos(\varphi_1 - \varphi_2)] - z_1[\cos \varphi_3 - \cos(\varphi_2 - \varphi_3)]\} = 0. \quad (14)$$

This equation, Equation (7) and the second closure condition (10) are a set of three homogeneous linear equations for  $z_1, z_2, z_3$ . Setting the coefficient determinant equal to zero results in

$$\left. \begin{aligned} A[\cos \varphi_1 - \cos(\varphi_1 - \varphi_2)] + B[\cos \varphi_3 - \cos(\varphi_2 - \varphi_3)] &= 0, \\ A &= 2m[\sin \varphi_2 - \sin \varphi_3 - \sin(\varphi_2 - \varphi_3)] - nC, \\ B &= 2m[\sin \varphi_1 - \sin \varphi_2 - \sin(\varphi_1 - \varphi_2)] + nC, \\ C &= \sin \varphi_1 - \sin \varphi_3 + \sin(\varphi_1 - \varphi_2) + \sin(\varphi_2 - \varphi_3) + 2 \sin(\varphi_3 - \varphi_1). \end{aligned} \right\} \quad (15)$$

This equation and the first closure condition (10) determine  $\varphi_1$  and  $\varphi_3$  as functions of  $\varphi_2$ . The angle  $\varphi_2$  can be chosen freely subject to the convexity condition (8). With angles  $\varphi_1, \varphi_2, \varphi_3$  thus determined Equation (7) and the second closure condition (10) determine  $z_1$  and  $z_3$  as functions of  $z_2$ . The coordinate  $z_2 \neq 0$  can be chosen freely subject to the condition that (11) yields a value  $r^2 > 0$ . Subsequently, Equations (3)–(6) determine  $d_1^2, a^2, b^2 = \ell^2$  and  $d_2^2$ .

The symmetry of deltoids has the effect that in both modes of deformation the same tiled PC is formed.

*Example 4.* A model made of cardboard conveyed the impression that the deltoid with parameters  $\ell = b = d_1 = d_2 = 1, a^2 = 2 - \sqrt{3}$  forms a tiled PC with  $m = 2, n = 3$ . This impression is shown to be wrong by solving Equations (2)–(7) and the first closure condition (10). The solutions  $\varphi_1 \approx -48.19306^\circ, \varphi_2 \approx 54.17303^\circ, \varphi_3 \approx 35.69159^\circ, z_1 \approx -.85198, z_2 \approx -.81181, z_3 \approx -.33690, r \approx .64121$  do not satisfy the second Equation (10).

In order to find an almost identical deltoid forming a tiled PC with  $m = 2, n = 3$  the almost identical values  $\varphi_2 = 54.18^\circ, z_2 = -.81$  are chosen. Equations(10) determine  $\varphi_3 - \varphi_1 = 83.88^\circ, M = 2000$  and  $z_3 - z_1 = .54$ . The remaining equations determine  $\varphi_1 \approx -48.18143^\circ, \varphi_3 \approx 35.69857^\circ, z_1 \approx -.872624, z_3 \approx -.332624, r \approx .655753$  and the desired parameters  $\ell = b \approx 1.023747, d_1 \approx 1.006381, d_2 \approx 1.029532, a \approx .521764$ . This tiled PC is formed by folding  $m + n = 5$  rows of deltoids. In Figure 6a it is shown in projection onto the  $y, z$ -plane.

◇

*Example 5.* The data  $m = 2, n = 1, \varphi_2 = 100^\circ, z_2 = 1$  determine a deltoid and the tiled PC formed by this deltoid. The closure conditions (10) determine  $\varphi_3 - \varphi_1 = 160^\circ, M = 18$  and  $z_3 - z_1 = -2$ . The remaining equations determine the parameters  $\varphi_1 \approx 44.3269^\circ, \varphi_3 \approx 204.3269^\circ, z_1 \approx .87156, z_3 \approx -1.12844, r \approx 1.56632, \ell = b \approx 1.46842, d_1 \approx 2.59976, a \approx 3.26361, d_2 \approx 3.67662$ . The tiled PC is formed by folding  $m + n = 3$  rows of deltoids. In Figure 6b it is shown in projection onto the  $y, z$ -plane.

◇

*Remark.* There are infinitely many more nonperiodic than periodic tiled PCs. However, there is no angle  $\varphi_2$  which is an irrational multiple of  $\pi$ , and for which Equation (15) and the first Equation (10) can be solved in nonnumerical form. Computers can handle only rational numbers. Hence the conclusion: Nonperiodic tiled PCs ( $M \rightarrow \infty$ ) exist, but examples cannot be given.

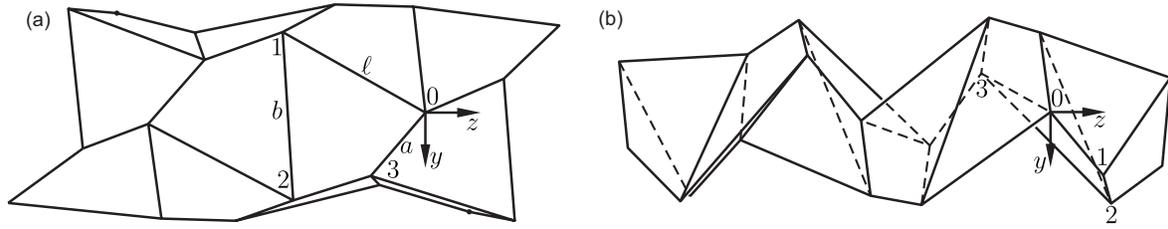
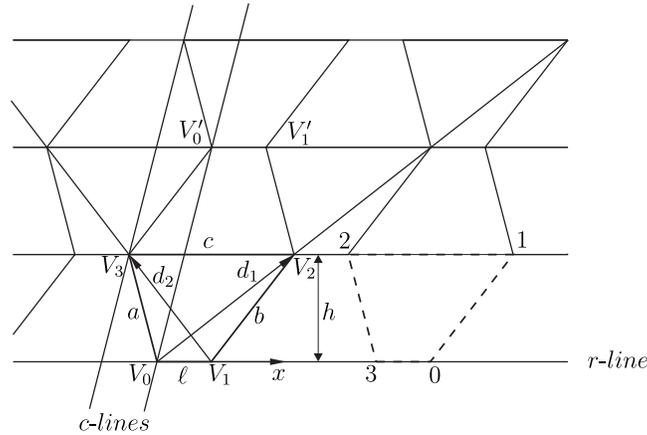


Figure 6: The foldable tiled PCs of Example 4 (Figure a) and Example 5 (Figure b).

Figure 7: Mesh composed of trapezoids. Parameters  $x_1, x_2, x_3, h$ .

## 6 Trapezoids

Figure 7 depicts a mesh composed of trapezoids with parallel sides  $V_0 - V_1$  and  $V_2 - V_3$ . As parameters of a single trapezoid the coordinates  $x_1, x_2, x_3$  of  $V_1, V_2, V_3$  and the height  $h$  are used (without loss of generality  $x_0 = 0, x_1 > 0$ ). In these terms the previously used parameters are

$$\ell = x_1, d_1^2 = h^2 + x_2^2, b^2 = h^2 + (x_2 - x_1)^2, a^2 = h^2 + x_3^2, d_2^2 = h^2 + (x_3 - x_1)^2. \quad (16)$$

### 6.1 Trivial Tiled Polyhedral Cylinders

Rows of trapezoids are separated by equidistant parallel straight lines which are the r-lines defined in Figure 1. One of the two modes of deformation is trivial. The mesh can be deformed with arbitrary fold angles along r-lines leaving rows planar. If identical fold angles are chosen, then all vertices of the mesh are located on a circular cylinder.

The PC is tiled if integers  $m$  and  $n$  exist such that the component of the vector  $m\vec{d}_1 + n\vec{d}_2$  along the r-lines equals zero, i.e., if  $mx_2 + n(x_3 - x_1) = 0$  (this is the second closure condition (10); the first closure condition does not apply). The condition is satisfied if the ratio  $q = (x_3 - x_1)/x_2$  is rational. Let  $(m, n)$  be a pair of integers with no common divisor satisfying the condition. Then the condition is satisfied by all  $(km, kn)$  with  $k = 1, 2, \dots$ . The cross section of a tiled PC with integers  $(km, kn)$  is a polygon with  $k(m + n)$  sides of length  $h$  inscribed in a circle. If this polygon is regular (irregular), then the tiled PC is foldable (self-intersecting).

Examples:

1.  $k(m + n) = 9$ : The cross section is either the regular polygon 1, 2, 3, 4, 5, 6, 7, 8, 9, 1 or the star 1, 3, 5, 7, 9, 2, 4, 6, 8, 1 or the star 1, 5, 9, 4, 8, 3, 7, 2, 6, 1.

2.  $k(m+n) = 14$ : The cross section is either the regular polygon 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 1 or the star 1, 4, 7, 10, 13, 2, 5, 8, 11, 14, 3, 6, 9, 12, 1 or the star 1, 6, 11, 2, 7, 12, 3, 8, 13, 4, 9, 14, 5, 10, 1.

## 6.2 Nontrivial Deformations

The second mode of deformation is nontrivial. Trapezoids inscribed in a circle are symmetric. For this reason the axial projections of the trapezoids  $V_0V_1V_2V_3$  and  $V_2V_3V'_0V'_1$  shown in Figure 7 coalesce. From this it follows that vertices which in the planar mesh are located on a c-line are located on a generator of the circular cylinder. This is expressed by the equation

$$\varphi_3 = \varphi_1 - \varphi_2. \quad (17)$$

The trapezoid drawn with dashed lines shows that in the trivial mode of deformation this equation is valid in the special form  $\varphi_3 = \varphi_1 - \varphi_2 = 0$ . With (16) and (17) Equations (2)–(7) are

$$2r^2(1 - \cos \varphi_1) + z_1^2 = x_1^2, \quad (18)$$

$$2r^2(1 - \cos \varphi_2) + z_2^2 = h^2 + x_2^2, \quad (19)$$

$$2r^2[1 - \cos(\varphi_1 - \varphi_2)] + z_3^2 = h^2 + x_3^2, \quad (20)$$

$$2r^2[1 - \cos(\varphi_1 - \varphi_2)] + (z_1 - z_2)^2 = h^2 + (x_2 - x_1)^2, \quad (21)$$

$$2r^2(1 - \cos \varphi_2) + (z_3 - z_1)^2 = h^2 + (x_3 - x_1)^2, \quad (22)$$

$$z_1[\sin \varphi_2 - \sin(\varphi_1 - \varphi_2) - \sin(2\varphi_2 - \varphi_1)] + (z_2 - z_3)[\sin \varphi_2 + \sin(\varphi_1 - \varphi_2) - \sin \varphi_1] = 0. \quad (23)$$

These equations are decoupled as follows. The difference of (19) and (22) and the difference of (20) and (21) read

$$(z_2 + z_3 - z_1)(z_2 - z_3 + z_1) = (x_2 + x_3 - x_1)(x_2 - x_3 + x_1), \quad (24)$$

$$(z_2 + z_3 - z_1)(z_3 - z_2 + z_1) = (x_2 + x_3 - x_1)(x_3 - x_2 + x_1). \quad (25)$$

The sum and the difference of these two equations are

$$z_1(z_2 + z_3 - z_1) = x_1(x_2 + x_3 - x_1), \quad (26)$$

$$(z_2 - z_3)(z_2 + z_3 - z_1) = (x_2 - x_3)(x_2 + x_3 - x_1), \quad (27)$$

whence it follows that with the given ratio of lengths of the parallel sides,  $\lambda = (x_2 - x_3)/x_1 > 0$ ,

$$(z_2 - z_3)/z_1 \equiv \lambda \text{ independent of } r. \quad (28)$$

$\lambda$  is independent of  $h$  and independent of whether the trapezoid is symmetric or not.

Equation (23) is a relationship between  $\varphi_1$  and  $\varphi_2$ :

$$\sin \varphi_2 - \sin(\varphi_1 - \varphi_2) - \sin(2\varphi_2 - \varphi_1) + \lambda[\sin \varphi_2 + \sin(\varphi_1 - \varphi_2) - \sin \varphi_1] = 0. \quad (29)$$

It has the solution  $\varphi_1 = \varphi_2$  associated with the trivial mode of deformation and a solution  $\varphi_1 \neq \varphi_2$  associated with the nontrivial mode of deformation. Explicit expressions are obtained by writing the equation in the form  $A \sin \varphi_1 + B \cos \varphi_1 = C$  with

$$A = [2 \cos \varphi_2 + (\lambda - 1)] \cos \varphi_2 - (\lambda + 1), \quad B = -[2 \cos \varphi_2 + (\lambda - 1)] \sin \varphi_2,$$

$$C = -(\lambda + 1) \sin \varphi_2, \quad A^2 + B^2 = 2(1 - \cos \varphi_2)(\lambda^2 + 1 + 2\lambda \cos \varphi_2),$$

$$R = \sqrt{A^2 + B^2 - C^2} = (\lambda - 1)(1 - \cos \varphi_2).$$

The solutions are  $\sin \varphi_1 = (AC \mp BR)/(A^2 + B^2)$ ,  $\cos \varphi_1 = (BC \pm AR)/(A^2 + B^2)$ . This yields  $\varphi_1 = \varphi_2$  and

$$\sin \varphi_1 = \frac{2(\lambda + \cos \varphi_2) \sin \varphi_2}{\lambda^2 + 1 + 2\lambda \cos \varphi_2}, \quad 1 - \cos \varphi_1 = \frac{2(1 - \cos^2 \varphi_2)}{\lambda^2 + 1 + 2\lambda \cos \varphi_2}, \quad (30)$$

$$\sin(\varphi_1 - \varphi_2) = \frac{(1 - \lambda^2) \sin \varphi_2}{\lambda^2 + 1 + 2\lambda \cos \varphi_2}, \quad 1 - \cos(\varphi_1 - \varphi_2) = \frac{(\lambda - 1)^2(1 - \cos \varphi_2)}{\lambda^2 + 1 + 2\lambda \cos \varphi_2}. \quad (31)$$

With these expressions and with  $x_3 = x_2 - \lambda x_1$  and  $z_3 = z_2 - \lambda z_1$  Equations (18)–(20) are

$$2r^2 \frac{2(1 - \cos^2 \varphi_2)}{\lambda^2 + 1 + 2\lambda \cos \varphi_2} + z_1^2 = x_1^2, \quad (32)$$

$$2r^2(1 - \cos \varphi_2) + z_2^2 = h^2 + x_2^2, \quad (33)$$

$$2r^2 \frac{(\lambda - 1)^2(1 - \cos \varphi_2)}{\lambda^2 + 1 + 2\lambda \cos \varphi_2} + (z_2 - \lambda z_1)^2 = h^2 + (x_2 - \lambda x_1)^2. \quad (34)$$

Equation (32) multiplied by  $\lambda^2$  plus Equation (33) minus Equation (34) is, following division by  $2\lambda$ ,

$$2r^2 \frac{(\lambda + 1)(1 - \cos^2 \varphi_2)}{\lambda^2 + 1 + 2\lambda \cos \varphi_2} - x_1 x_2 = -z_1 z_2. \quad (35)$$

Squaring and eliminating  $z_1^2 z_2^2$  by means of (32) and (33) results in

$$\left[ 2r^2 \frac{(\lambda + 1)(1 - \cos^2 \varphi_2)}{\lambda^2 + 1 + 2\lambda \cos \varphi_2} - x_1 x_2 \right]^2 = \left[ x_1^2 - 2r^2 \frac{2(1 - \cos^2 \varphi_2)}{\lambda^2 + 1 + 2\lambda \cos \varphi_2} \right] \left[ h^2 + x_2^2 - 2r^2(1 - \cos \varphi_2) \right]. \quad (36)$$

This is a fourth-order equation for  $\cos \varphi_2$  with parameter  $r$ . For  $y = 2r^2$  it is the quadratic equation  $Py^2 - Qy = -h^2 x_1^2$  with

$$P = \left[ \frac{(\lambda - 1)(1 - \cos \varphi_2) \sin \varphi_2}{\lambda^2 + 1 + 2\lambda \cos \varphi_2} \right]^2,$$

$$Q = \frac{1 - \cos \varphi_2}{\lambda^2 + 1 + 2\lambda \cos \varphi_2} \left\{ 2(1 + \cos \varphi_2) \left[ h^2 + \left( x_2 - x_1 \frac{\lambda + 1}{2} \right)^2 \right] + \frac{1}{2} x_1^2 (\lambda - 1)^2 (1 - \cos \varphi_2) \right\} > 0.$$

Both roots  $y = (Q \pm \sqrt{Q^2 - 4h^2 x_1^2 P})/(2P)$  are real and positive since

$$Q^2 - 4h^2 x_1^2 P = \frac{4 \sin^4 \varphi_2}{(\lambda^2 + 1 + 2\lambda \cos \varphi_2)^2} F_1 F_2,$$

$$F_{1,2} = \left[ h \pm x_1 \frac{(\lambda - 1) \sin \varphi_2}{2(1 + \cos \varphi_2)} \right]^2 + \left[ x_2 - x_1 \frac{\lambda + 1}{2} \right]^2 > 0.$$

Only with the smaller of the roots  $2r^2$  Equations (32) and (33) yield quantities  $z_1^2 > 0$  and  $z_2^2 > 0$ .

For angles  $\varphi_1, \varphi_2 \ll 1$  Taylor expansion of (30) and (36) yields the approximations

$$\varphi_2 \approx \frac{\lambda + 1}{2} \varphi_1, \quad r\varphi_1 \approx x_1 \frac{h}{\sqrt{h^2 + [x_2 - x_1(\lambda + 1)/2]^2}} = \text{const.} \quad (37)$$

The square root is the distance between the midpoints of the parallel sides of the trapezoid.  $r\varphi_1 \approx x_1$  if the trapezoid is symmetric.

### 6.3 Geometrical Solution

Nontrivial states of deformation are constructed as shown in Figure 3. Equation (9) reads

$$\det \begin{bmatrix} x^2 & y^2 & xy & y \\ x_2^2 & h^2 & x_2h & h \\ x_3^2 & h^2 & x_3h & h \\ x_4^2 & y_4^2 & x_4y_4 & y_4 \end{bmatrix} - x_1 \cdot \det \begin{bmatrix} y^2 & xy & x & y \\ h^2 & x_2h & x_2 & h \\ h^2 & x_3h & x_3 & h \\ y_4^2 & x_4y_4 & x_4 & y_4 \end{bmatrix} = 0.$$

This is the equation

$$\left. \begin{aligned} A(x^2 - x_1x) + 2Bxy + Cy^2 + Ey &= 0, \\ A &= h^2(x_2 - x_3)(y_4^2 - hy_4), \quad 2B = -h(x_2 - x_3)(x_2 + x_3 - x_1)(y_4^2 - hy_4), \\ C &= -h(x_2 - x_3)[h(x_4^2 - x_1x_4) - (x_2 + x_3 - x_1)x_4y_4 + x_2x_3y_4], \\ E &= h(x_2 - x_3)[h^2(x_4^2 - x_1x_4) - h(x_2 + x_3 - x_1)x_4y_4 + x_2x_3y_4^2]. \end{aligned} \right\} \quad (38)$$

The fourth-order equation  $AC - B^2 = 0$  separating ellipses and hyperbolas is

$$(y_4^2 - hy_4)(A^*x_4^2 + 2B^*x_4y_4 + C^*y_4^2 + D^*x_4 + E^*y_4) = 0 \quad (39)$$

with coefficients  $A^* = h^2$ ,  $2B^* = -h(x_2 + x_3 - x_1)$ ,  $C^* = (x_2 + x_3 - x_1)^2/4$  satisfying the equation  $A^*C^* - B^{*2} = 0$ . Equation (39) is the equation of the parallel lines  $y_4 = 0$  and  $y_4 = h$  and of the single parabola passing through the vertices of the trapezoid (see [1, Example 7.4.1]).

Let  $\Delta_1$  be the domain inside the parabola,  $\Delta_2$  be the domain between the parallel lines and  $\Delta_{12}$  be the intersection of  $\Delta_1$  and  $\Delta_2$ . Equation (38) determines an ellipse if the point  $(x_4, y_4)$  is located either in  $\Delta_1$  or in  $\Delta_2$ , but not in  $\Delta_{12}$ . Every ellipse is located in  $\Delta_1$  as well as in  $\Delta_2$ . The semi axes  $b$  of these ellipses are in the range  $h/2 < b < \infty$ . Since there are no ellipses in the trivial mode of deformation, every ellipse determines a nontrivial deformation of the mesh. The lines  $y_4 = 0$  and  $y_4 = h$  determine a trivial deformation.

### 6.4 Nontrivial Tiled Polyhedral Cylinders

Because of (17) the closure conditions (10) are

$$\varphi_1 - \varphi_3 = \varphi_2 = 2\pi/(m - n), \quad mz_2 + n(z_3 - z_1) = 0. \quad (40)$$

The first condition tells that (i) integers  $(m, n)$  with  $m - n = 0$  or  $\pm 1$  can occur only in tiled PCs in the trivial mode of deformation and that (ii) nontrivial tiled PCs are M-periodic with  $M = |m - n|$ .

Nontrivial tiled PCs can be constructed as follows. Given are

1. Arbitrary integers  $m, n$  ( $m - n \neq 0, \pm 1$ ) and arbitrary angles  $\varphi_1, \varphi_2, \varphi_3$  satisfying Equations (40),
2. one of the coordinates  $z_1, z_2, z_3$  ( $\neq 0$  arbitrary),
3. either one of the parameters  $r, \ell, d_1, a, b, d_2$  or one of the parameters  $r, x_1, x_2, x_3, h$ .

The unknowns among  $z_1, z_2, z_3$  are determined by Equation (7) and by the second Equation (40). The unknowns among the parameters  $r, \ell, d_1, a, b, d_2$  are determined by Equations (2)–(6). The unknowns among the parameters  $r, x_1, x_2, x_3, h$  are determined by Equations (35), (28) and (19). If  $r$  is not prescribed, then the prescribed parameter must be sufficiently large so as to determine a value  $r^2 > 0$ .

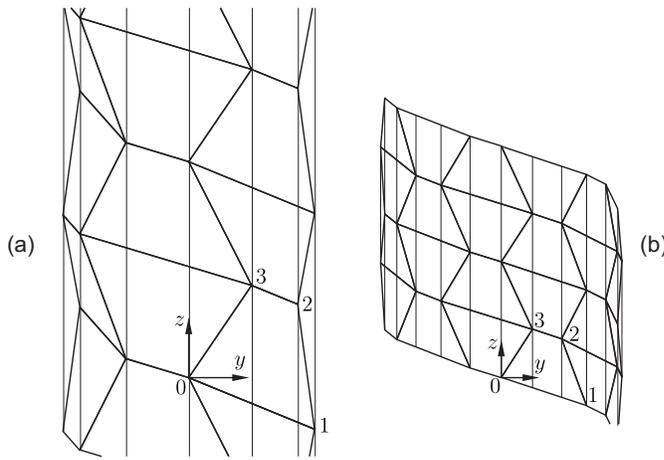


Figure 8: Foldable tiled PCs of Example 6 with the parameters (a) and (b).

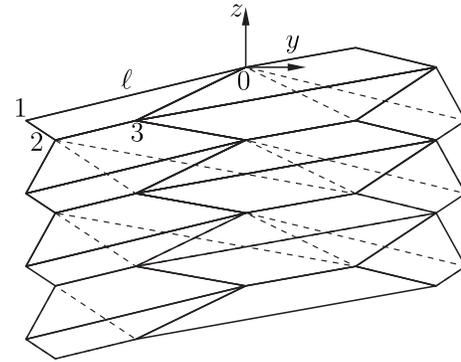


Figure 9: Foldable tiled PC of Example 7.

*Example 6.* Given are the two sets of parameters

(a)  $m = 4, n = -2, \varphi_1 = 90^\circ, x_1 = 1, z_3 = 1/2,$

(b)  $m = 8, n = -4, \varphi_1 = 45^\circ, x_1 = 1/2, z_3 = 1/4.$

Note that  $m$  and  $n$  in (b) are twice as large as in (a) while  $\varphi_1, x_1, z_3$  in (a) are twice as large as in (b).

Solution to Problem (a):  $M = 6, \varphi_2 = 60^\circ, \varphi_3 = 30^\circ, z_1 = -\sqrt{3}/6 \approx -.2887, z_2 = (3 + \sqrt{3})/12 \approx .3943, \lambda = (\sqrt{3} - 1)/2 \approx .3660, r^2 = 11/24, r \approx .6770, x_2 = 3(1 + \sqrt{3})/16 \approx .5123, x_3 = (11 - 5\sqrt{3})/16 \approx .1462, h^2 = 11(14 - \sqrt{3})/384, h \approx .5928, q = (x_3 - x_1)/x_2 = -5/3.$

The tiled PC is formed by folding  $m - n = 6$  columns of trapezoids. In Figure 8a it is shown in projection onto the  $y, z$ -plane. The result for  $q$  shows that with the same mesh tiled PCs in the trivial mode of deformation can be formed with integers  $(m^*, n^*) = (5k, 3k)$  ( $k = 1, 2, \dots$ ).

Solution to Problem (b):  $M = 12, \varphi_2 = 30^\circ, \varphi_3 = 15^\circ, z_1 = -(2 + 5\sqrt{2} - 3\sqrt{3} + 4\sqrt{6})/92 \approx -.1486, z_2 = (25 + 5\sqrt{2} - 3\sqrt{3} + 4\sqrt{6})/184 \approx .1993, \lambda = (1 + \sqrt{2} - \sqrt{3})/2 \approx .3411, 2r^2 = (3982 + 2043\sqrt{2} - 108\sqrt{3} - 40\sqrt{6})/92^2, r \approx .6238, x_2 = (5679 + 1927\sqrt{2} - 2113\sqrt{3} - 234\sqrt{6})/(2 \cdot 92^2) \approx .2464, x_3 = (1447 - 2305\sqrt{2} + 2119\sqrt{3} - 234\sqrt{6})/(2 \cdot 92^2) \approx .0759, h^2 = 2r^2(1 - \sqrt{3}/2) + z_2^2 - x_2^2, h \approx .2885.$

The tiled PC is formed by folding  $m - n = 12$  columns of trapezoids. In Figure 8b it is shown in projection onto the  $y, z$ -plane. The scale is the same as in Figure 8a. Since  $q = (x_3 - x_1)/x_2$  is irrational no tiled PC can be formed in the trivial mode of deformation.  $\diamond$

*Example 7.* Given are  $m = 0, n = 6, \varphi_1 = -90^\circ, z_1 \neq 0$  arbitrary,  $d_2$  arbitrary. Definition:  $\mu = z_1^2/d_2^2$ . The parameters of the tiled PCs determined by these data are  $M = 6, \varphi_2 = -60^\circ, \varphi_3 = -30^\circ, z_2 = z_1(\sqrt{3} + 1)/2, z_3 = z_1, \lambda = (\sqrt{3} - 1)/2, r = d_2, \ell^2 = d_2^2(2 + \mu), d_1^2 = d_2^2[1 + \mu(1 + \sqrt{3}/2)], a^2 = d_2^2(2 - \sqrt{3} + \mu), b^2 = d_2^2(2 - \sqrt{3})(1 + \mu/2), q = -1/(1 + \mu).$

In Figure 9 the foldable tiled PC with the parameters  $z_1 = -1/2, d_2 = 2$  is shown in projection onto the  $y, z$ -plane. From  $z_3 = z_1$  and  $(m, n) = (0, 6)$  it follows that every string of six diagonals  $d_2$  connecting two vertices in the planar mesh is mapped into a regular hexagon in a plane  $z = \text{const}$ . One out of six trapezoids is seen edge-on. From  $q = -16/17$  it follows that with the same mesh tiled PCs in the trivial mode of deformation can be formed with integers  $(m^*, n^*) = (16k, 17k)$  ( $k = 1, 2, \dots$ ).  $\diamond$

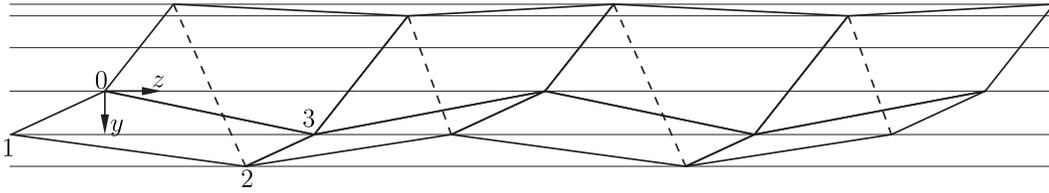


Figure 10: Foldable tiled PC of Example 8.

*Example 8.* The data  $m = 2$ ,  $n = -1$ ,  $\varphi_1 = 150^\circ$ ,  $z_1 = -1$ ,  $r = 1$  determine the tiled PC with the parameters  $M = 3$ ,  $\varphi_2 = 120^\circ$ ,  $\varphi_3 = 30^\circ$ ,  $z_2 = \sqrt{3}$ ,  $z_3 = 2\sqrt{3} - 1$ ,  $\lambda = \sqrt{3} - 1$ ,  $\ell^2 = 3 + \sqrt{3}$ ,  $d_1^2 = 6$ ,  $a^2 = 5(3 - \sqrt{3})$ ,  $b^2 = 6 + \sqrt{3}$ ,  $d_2^2 = 15$ ,  $h^2 = 3(13 + \sqrt{3})/8$ ,  $q = 1 - 2\sqrt{3}$ .

In Figure 10 the tiled PC is shown in projection onto the  $y, z$ -plane. It is formed by folding  $m - n = 3$  columns of quadrilaterals. Since  $q$  is irrational no tiled PC can be formed in the trivial mode of deformation.  $\diamond$

### 6.5 Symmetric Trapezoids

A symmetric trapezoid is specified by the parameters  $x_1 = \ell$ ,  $x_2 - x_3 = c$  and  $h$ . The symmetry has the effect that c-lines are orthogonal to r-lines. The closure condition  $mx_2 + n(x_3 - x_1) = 0$  is satisfied by all integers  $(m, n = m)$  with  $m = 2, 3, \dots$ . Hence infinitely many trivial tiled PCs can be formed.

In what follows, it is shown that also infinitely many nontrivial tiled PCs can be formed. The orthogonality of r-lines and c-lines is preserved when the mesh is deformed. Edges of alternating length  $\ell$ ,  $c$ ,  $\ell$ ,  $c$  etc. on an r-line are mapped into secants of the circle of radius  $r$  (arbitrary) in a plane  $z = \text{const}$ . In particular,  $z_1 = 0$  and  $z_2 = z_3$  independent of  $r$ . With this, the second condition (40) is satisfied. The PC is tiled if  $m \geq 2$  pairs of secants  $(\ell, c)$  form a regular polygon. This requires  $n = -m$ . With this, the first condition (40) reads  $\varphi_1 - \varphi_3 = \varphi_2 = \pi/m$ . The angle  $\varphi_1$  and the radius  $r$  as functions of  $m$  are determined by Equation (30) and by Equation (35) with  $z_1 = 0$ ,  $x_1x_2 = \ell(\lambda + 1)/2$ . The results are, independent of  $h$ ,

$$\varphi_2 = \frac{\pi}{m}, \quad \sin \varphi_1 = \frac{2(\lambda + \cos \varphi_2) \sin \varphi_2}{\lambda^2 + 1 + 2\lambda \cos \varphi_2}, \quad \varphi_3 = \varphi_1 - \varphi_2, \quad r = \frac{\ell}{2} \frac{\sqrt{\lambda^2 + 1 + 2\lambda \cos \varphi_2}}{\sin \varphi_2} \quad (41)$$

( $m = 2, 3, \dots$ ) Only fold angles along edges depend on  $h$ .

### Summary

A Kokotsakis mesh formed by congruent convex, non-trapezoidal, non-parallelogramic quadrilaterals is a single-degree-of-freedom mechanism with two modes of deformation. In both modes the mechanism is a polyhedral cylinder (PC) since the vertices of all quadrilaterals are located on a circular cylinder the radius  $r$  of which is a free parameter. In Section 2 six equations are formulated for six cylinder coordinates  $\varphi_k, z_k$  ( $k = 1, 2, 3$ ) as functions of  $r$ . These equations depend on five parameters specifying the quadrilaterals. The equations can only be solved numerically.

In Section 3 a simple geometrical method of solution is shown. It leads to equations of the two parabolas passing through the vertices of a convex quadrilateral and to an algorithm

determining the smallest radius  $r$  for which the six equations for  $\varphi_k, z_k$  ( $k = 1, 2, 3$ ) have real solutions.

In Section 4 it is shown that tiled PCs with coordinates  $r, \varphi_k, z_k$  ( $k = 1, 2, 3$ ) exist if two additional equations with two additional unknown integers  $m, n$  are satisfied. Necessary conditions on the five parameters for the existence of a solution are not available. The construction of tiled PCs is explained. Tiled PCs are either foldable or self-intersecting. They are periodic if  $\varphi_2/\pi$  is rational.

In Section 5 a two-parametric family of deltoids forming tiled PCs with prescribed integers  $(m, n)$  is determined. In both modes of deformation the same tiled PC is formed.

Section 6 is devoted to trapezoidal quadrilaterals. In this case, the six equations for  $\varphi_k, z_k$  ( $k = 1, 2, 3$ ) are decoupled. The two modes of deformation are distinguished as trivial and nontrivial. For both modes the construction of tiled PCs is explained. Nontrivial tiled PCs are periodic. Symmetric trapezoids form in both modes infinitely many tiled PCs.

An open problem: Are there non-deltoidal, non-trapezoidal quadrilaterals forming tiled PCs in both modes of deformation?

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